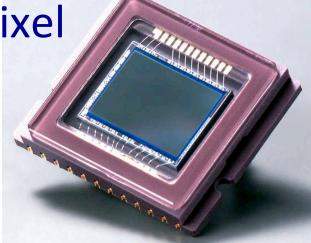
# Anatomy of a CCD pixel

- Coatings to minimize reflection off outer surface
- Can operate upside down (*backside illumination*) if the CCD is *thinned*
  - Generally more expensive
  - Higher QE because no gate structures in the way
  - Less absorption of red photons (because thinner)
  - Potential non-uniform thickness must be calibrated



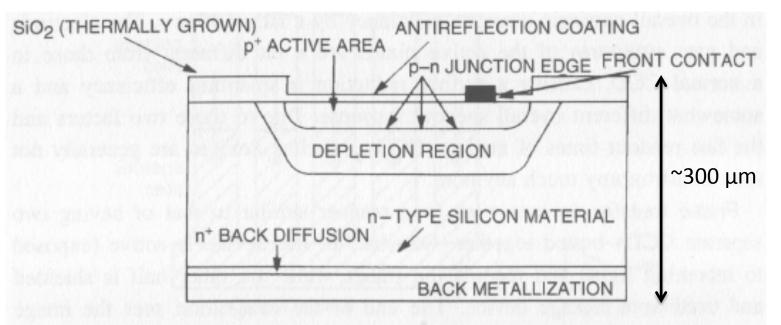


Fig. 2.4. Schematic view of a single front-side illuminated CCD pixel. The square labeled "front contact" is a representation of part of the overall gate structure. The letters "p" and "n" refer to regions within the pixel consisting of silicon doped with phosphorus and boron respectively.

## Front-side vs. back-side (thinned) CCDs

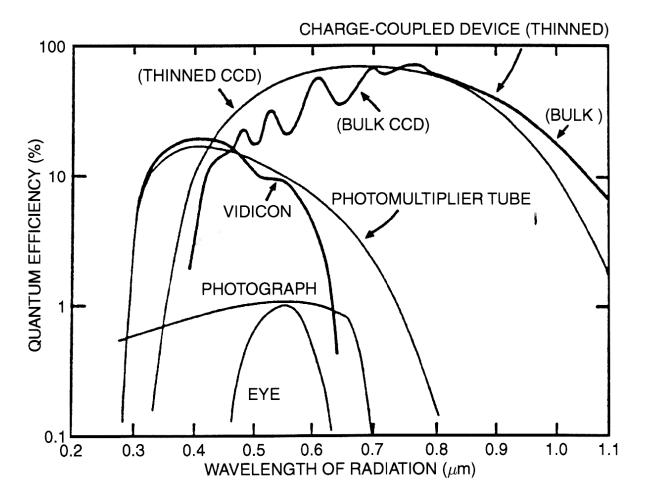
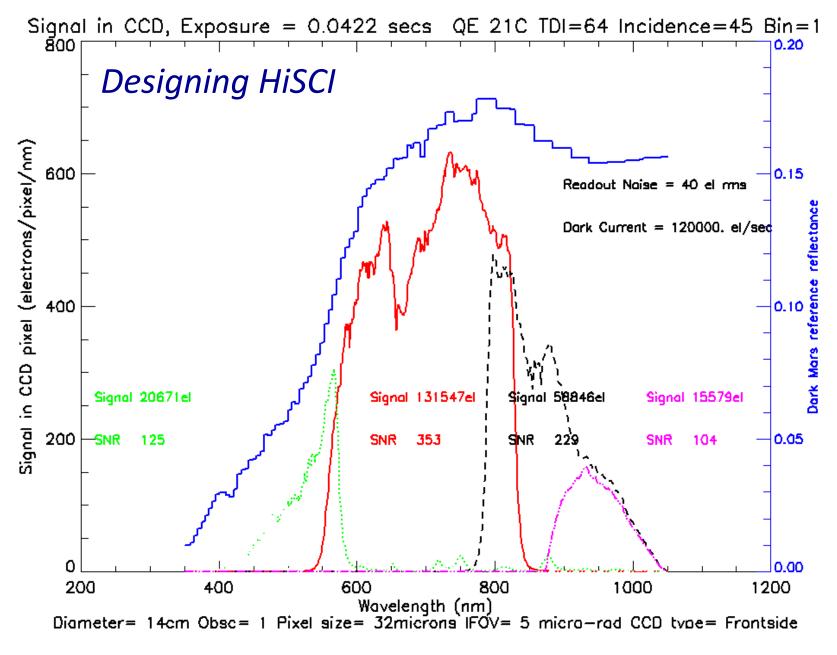
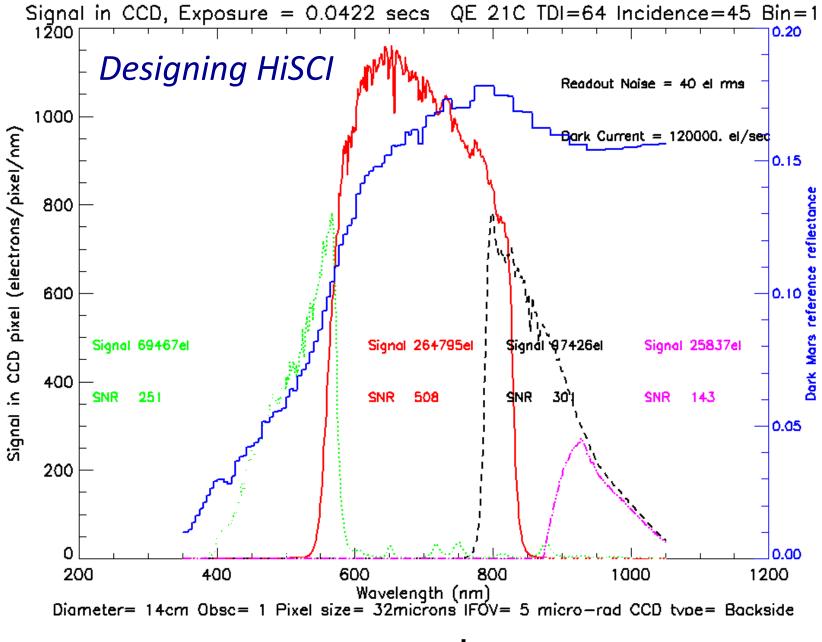


Fig. 3.2. QE curves for various devices, indicating why CCDs are a quantum leap above all previous imaging devices. The failure of CCDs at optical wavelengths shorter than about 3500 Å has been essentially eliminated via thinning or coating of the devices (see Figure 3.3).

#### One of the keys to HiRISE's excellent S/N: back-side illumination



2010 Frontside QE data



2010 Backside QE data – Morley's Model

# Coatings can boost blue/UV absorptivity

Generally a phosphorescent material that "converts" UV photons into detectable longer-wavelength photons

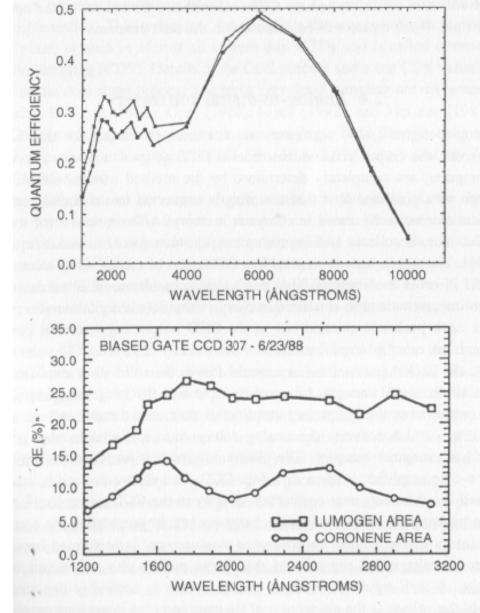


Fig. 2.9. The top plot shows QE curves for a Hubble Space Telescope WF/PC prototype CCD before and after being coated with lumogen. Note the increased UV response of the coated CCD. The bottom plot shows the QE properties of a WF/PC prototype in the far-UV spectral region. Presented are two curves, one for a coronene coated CCD and one for a lumogen coated CCD. From Trauger (1990).

## Coatings can boost blue/UV absorptivity

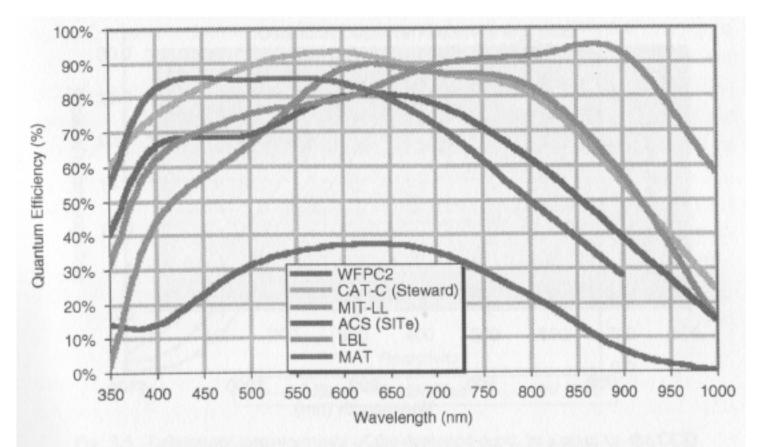
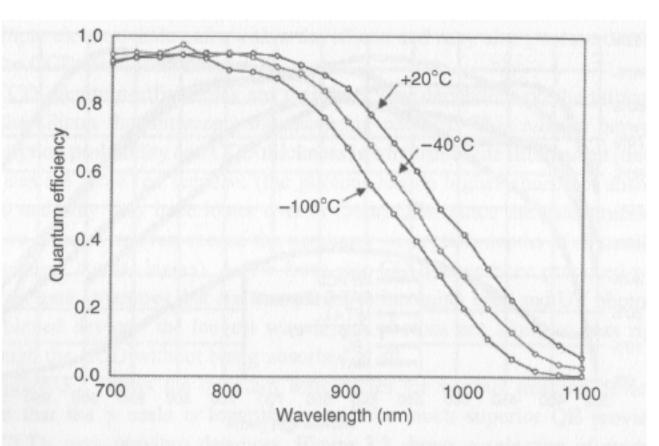
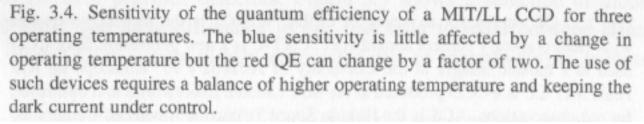


Fig. 3.3. QE curves for a variety of CCDs. WFPC2 is the second generation wide-field/planetary camera aboard HST, CAT-C is a new generation SITe CCD used in a mosaic imager at the University of Arizona's 90" telescope on Kitt Peak, MIT-LL is a CCD produced at the MIT Lincoln Laboratories and optimized for red observations, ACS is the Hubble Space Telescope Advanced Camera for Surveys SITe CCD, LBL is a Lawrence Berkeley Lab high resistivity, "deep depletion" CCD with high red QE, and MAT is a front-side, processed CCD showing high blue QE.

#### QE also depends on temperature (higher $T \rightarrow$ higher QE ... but also higher noise)





#### QE also depends on temperature (higher $T \rightarrow$ higher QE ... but also higher noise — dark current)

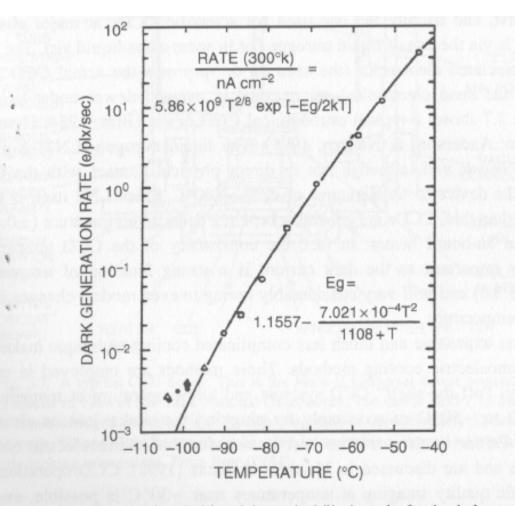
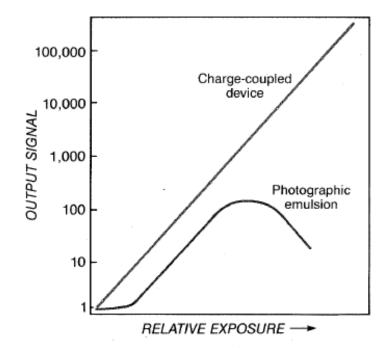


Fig. 3.6. Experimental (symbols) and theoretical (line) results for the dark current generated in a typical three-phase CCD. The rate of dark current, in electrons generated within each pixel every second, is shown as a function of the CCD operating temperature.  $E_g$  is the band gap energy for silicon. From Robinson (1988a).

#### CCDs have exceptionally good linearity...



CCD's are exceptionally linear; doubling the exposure yields a signal exactly twice as strong. This holds over an enormous exposure range, enabling CCD's to detect simultaneously very bright and very faint objects in a single image. This behavior contrasts strikingly with that of photographic emulsions, which are only linear over a narrow range of exposure. Emulsions must also overcome a threshold before they start to form an image at all. Worse, beyond a certain point emulsions saturate; their ability to detect light actually decreases if the exposure is too long.

## ...until you approach the full well capacity

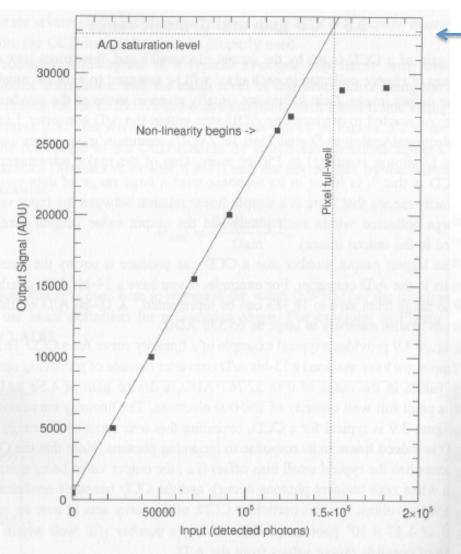


Fig. 3.9. CCD linearity curve for a typical three-phase CCD. We see that the device is linear over the output range from 500 ADU (the offset bias level of the CCD) to 26 000 ADU. The pixel full well capacity is 150 000 electrons and the A/D converter saturation is at 32 767 ADU. In this example, the CCD nonlinearity is the limiting factor of the largest usable output ADU value. The slope of the linearity curve is equal to the gain of the device.

HiRISE is 14-bit, so A/D saturation at half this DN

...and there can be deviations even before that

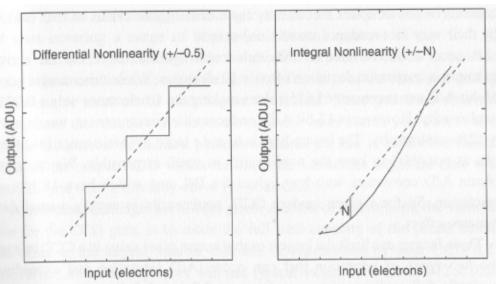


Fig. 3.10. The two types of CCD nonlinearity are shown here in cartoon form. Differential nonlinearity (left) comes about due to the finite steps in the A/D conversion process. Here we see that the linearity curve (dashed line) cuts through each step at the halfway point yielding a DNL of  $\pm 0.5$  ADU. Integral nonlinearity (right) is more complex and the true linearity curve (solid line) may have a simple or complex shape compared with the measured curve (dashed line). A maximum deviation (N) is given as the INL value for an A/D and may occur anywhere along the curve and be of either sign. Both plots have exaggerated the deviation from linearity for illustration purposes.

## **Deviations from CCD linearity**

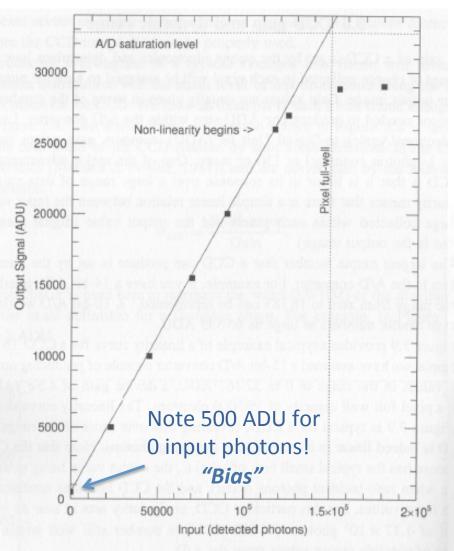


Fig. 3.9. CCD linearity curve for a typical three-phase CCD. We see that the device is linear over the output range from 500 ADU (the offset bias level of the CCD) to 26 000 ADU. The pixel full well capacity is 150 000 electrons and the A/D converter saturation is at 32 767 ADU. In this example, the CCD nonlinearity is the limiting factor of the largest usable output ADU value. The slope of the linearity curve is equal to the gain of the device.

What's a simple way to check your CCD's linearity?

Integrate for 1 second, 2 seconds, 4 seconds, ...

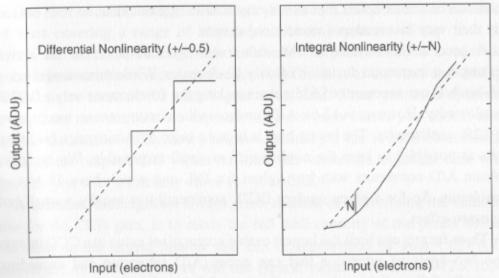


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# Measuring the bias

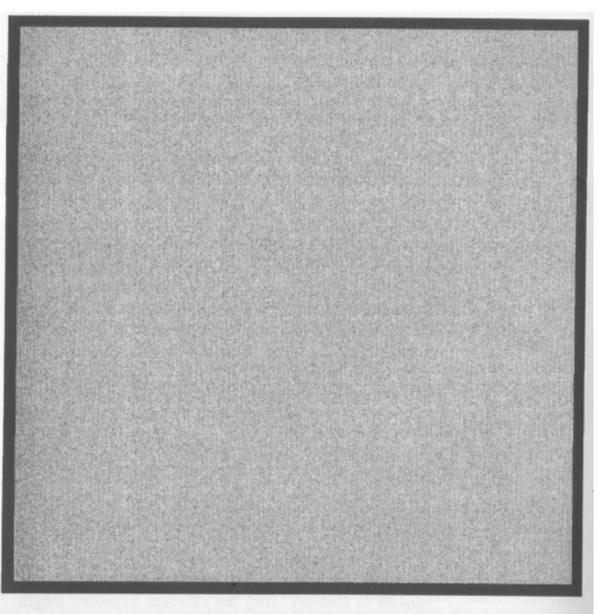


Fig. 4.2. Shown is a typical CCD bias frame. The histrogram of this image was shown in Figure 3.8. Note the overall uniform structure of the bias frame.

- A/D conversion purposely includes offset (bias) such that  $0 e^{-} \rightarrow > 0 DN$
- Measure the bias by reading out "image" acquired with integration time of 0 seconds

## Bias is used because of *read noise*

 Amplifier, A/D converter, electronics don't give perfectly repeatable results; i.e. the same pixel detecting the same radiance will yield distribution of DNs varying by ~ a few e<sup>-</sup>

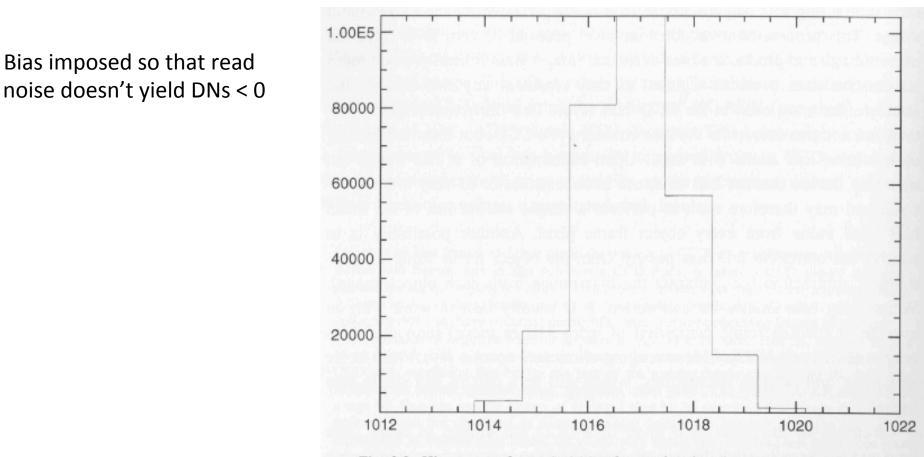
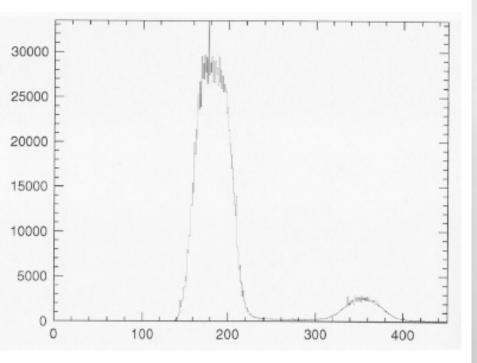


Fig. 3.8. Histogram of a typical bias frame showing the number of pixels vs. each pixel ADU value. The mean bias level offset or pedestal level in this Loral CCD is near 1017 ADU, and the distribution is very Gaussian in nature with a FWHM value of near 2 ADU. This CCD has a read noise of 10 electrons and a gain of  $4.7 e^{-}/ADU$ .

## Dark current

• Thermal noise

Can vary from pixel to pixel



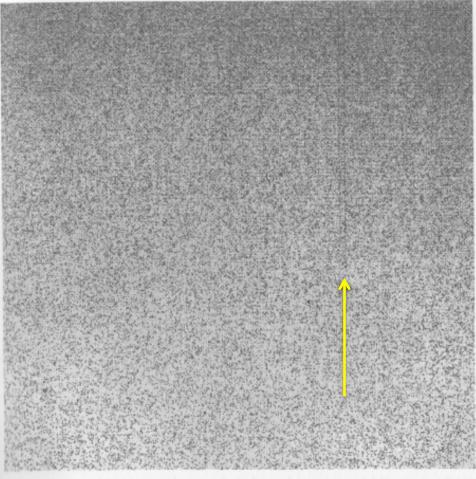
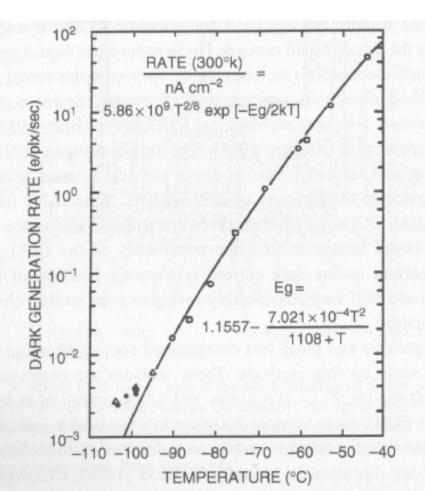


Fig. 4.3. Shown is a typical CCD dark frame. This figure shows a dark frame for a Kodak CCD operating in MPP mode and thermoelectrically cooled. Notice the nonuniform dark level across the CCD, being darker (greater ADU values) on the top. Also notice the two prominent partial columns with higher dark counts, which extend from the top toward the middle of the CCD frame. These are likely to be column defects in the CCD that occurred during manufacture, but with proper dark subtraction they are of little consequence. The continuation of the figure shows the histogram of the dark frame. Most of the dark current in this 180 second exposure is uniformly distributed near a mean value of 180 ADU with a secondary maximum near 350 ADU. The secondary maximum represents a small number of CCD pixels that have nearly twice the dark current of the rest, again most likely due to defects in the silicon lattice. As long as these increased dark current pixels remain constant, they are easily removed during image calibration.

# Dark current

 Negligible when cooled to near liquid N temperatures (77 K)



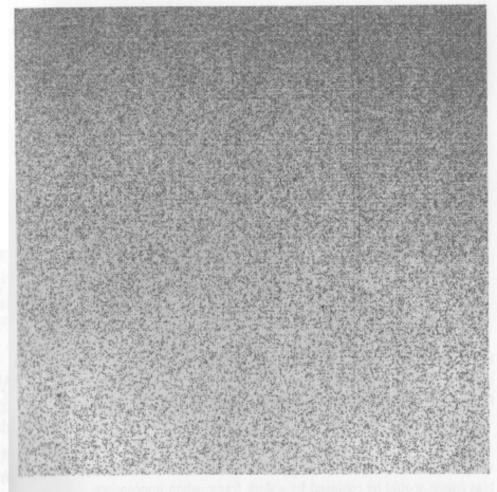
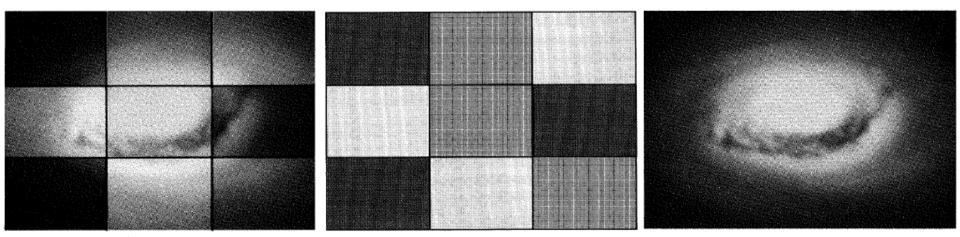


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#### Also need to account for varying pixel sensitivity



This simulated "raw" image from a chargecoupled device does not give a realistic representation of the well-known Blackeye galaxy, M64 in Coma Berenices, because individual pixels have varying sensitivities to light. This effect is shown here schematically by dividing the image into nine regions of grossly different sensitivities. Images such as this are obviously not very useful to astronomers or anybody else. To overcome this nonuniformity problem, observers use a technique called flat-fielding. During an observing run an exposure is made of a uniform source such as the dawn sky or inside of the telescope dome to map the variations among the CCD's pixels. This image represents the flat-field frame corresponding to the simulated raw image of the Black-eye galaxy shown above. Once the response of each pixel is known, observers can scale the data by an amount determined from the flat-field exposure and thereby correct for each pixel's individual response. The result is the same as that which would be registered by a CCD with pixels of identical sensitivity; it can now be analyzed by astronomers. Image courtesy Rudolph Schild.

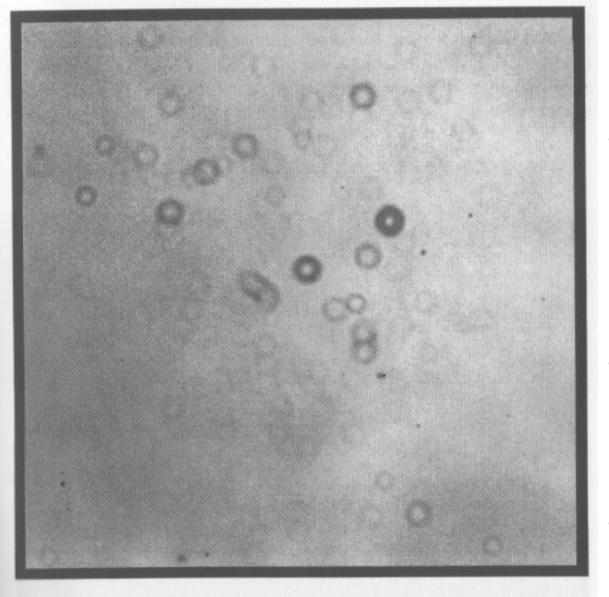


Fig. 4.4. Shown is a typical CCD flat field image. This is an R-band flat field image for a  $1024 \times 1024$  Loral CCD. The numerous "doughnuts" are out of focus dust specks present on the dewar window and the filter. The varying brightness level and structures are common in flat field images. As seen in the histogram of this image (Figure 4.1) this flat field has a mean level near 6950 ADU, with an approximate dispersion of (FWHM) 400 ADU.

# Flat field images

- Illuminate detector
  uniformly, preferably with
  color spectrum similar to
  what you actually want to
  image
- Note dust specs on detector surface, and "low spatial frequency" variations
- With telescopes, point at dome wall or white screen; not so easy with instruments in space...

#### Bottom line of image processing ("data reduction")

Final Reduced Object Frame =  $\frac{\text{Raw Object Frame} - \text{Bias Frame}}{\text{Flat Field Frame}}$ 

• Replace "Bias" with "Dark" if not at extremely low temperature (dark image will include the bias anyway)

• "Flat Field Frame" assumed to also be Bias/Dark-subtracted

#### The all-important *signal-to-noise ratio*

• Estimate from the "CCD Equation":

$$\frac{\mathrm{S}}{\mathrm{N}} = \frac{N_*}{\sqrt{N_* + n_{\mathrm{pix}}(N_S + N_D + N_R^2)}}$$

- N<sub>\*</sub> = photons (or equivalent e<sup>-</sup>) from target object(s)
- $n_{pix} = #$  of pixels
- $N_s$  = photons/e<sup>-</sup> from "background" ("empty" sky in astronomy)
- N<sub>D</sub> = dark current
- $N_R$  = read noise

Note that if  $N_* >>$  the noise terms, then S/N ~  $\vee(N_*)$ 

Increases as square root of integration time:

$$\frac{\mathrm{S}}{\mathrm{N}} = \frac{Nt}{\sqrt{Nt + n_{\mathrm{pix}} \left(N_{S}t + N_{D}t + N_{R}^{2}\right)}}$$